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基于相变材料的宽带高消光比非易失性光开关

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摘要:本文介绍了一种基于相变材料 Sb_2Se_3 的宽带、高消光比、非易失的 2×2 马赫-增德尔干涉仪(MZI)型光开关。在波长为 1550 nm 时,插入损耗 (IL) 为 0.84 dB,消光比 (ER) 达到 28.8 dB。器件的 3 dB 带宽大于 150 nm。在 3 dB 带宽内,直通态和交叉态的消光比分别大于 20.3 dB 和 16.3 dB。 Sb_2Se_3 的晶化和非晶化功耗分别为 105.86 nJ 和 49 nJ。该宽带高消光比非易失性光开关在光互连和光计算中有极大的应用潜力。

关键词:光子集成;光开关;相变材料

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Broadband high-extinction-ratio nonvolatile optical switch based on phase change material

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Abstract: In this paper, we present a broadband, high-extinction-ratio, nonvolatile 2×2 Mach-Zehnder interferometer (MZI) optical switch based on the phase change material Sb_2Se_3 . The insertion loss (IL) is 0. 84 dB and the extinction ratio (ER) reaches 28. 8 dB at the wavelength of 1550 nm. The 3 dB bandwidth is greater than 150 nm. Within the 3 dB bandwidth, the ER is greater than 20. 3 dB and 16. 3 dB at bar and cross states, respectively. The power consumption for crystallization and amorphization of Sb_2Se_3 is 105. 86 nJ and 49 nJ, respectively. The switch holds significant promise for optical interconnects and optical computing applications.

Key words: photonic integration, optical switch, phase change materials **PACS:**

Introduction

With the rapid development of artificial intelligence, data traffic is experiencing exponential growth^[1,2]. The demand for parallelism and data bandwidth is increasing, and reducing power consumption and economic costs is becoming more critical. Optical data transmission offers advantages over traditional electrical signals in high-speed, high-bandwidth applications^[3]. Optical switches are one of the fundamen-

tal components in integrated photonic circuits, functioning to perform physical switching and logical operations on optical signals in transmission lines or integrated photonic circuits. The Mach–Zehnder interferometer (MZI) is a common structure in optical switches. It offers advantages such as wide operational bandwidth, low loss, high fabrication tolerance, and insensitivity to temperature^[4]. Traditional MZI silicon–based optical switches typically achieve switching functionality

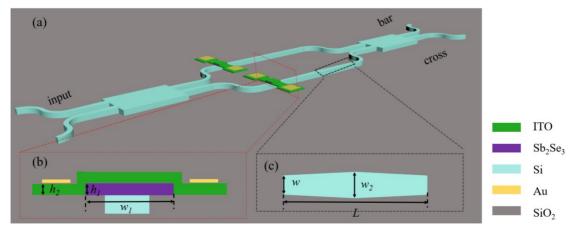
by altering the effective refractive index of optical modes through the thermo-optic effect or plasma dispersion effect. However, optical modulation based on the plasma dispersion effect or thermo-optical effect is weak (usually $\Delta n < 0.01$) [5], which results in large footprint or high power consumption. Moreover, silicon-based thermo-optical and electro-optical switches require continuous energy to maintain ON/OFF state, which makes high static power consumption.

Phase change materials (PCMs) have attracted a lot of attention due to its excellent properties, such as high refractive index contrast between crystalline and amorphous states, nonvolatility, reversibility and high repeatability^[6-10]. Ge₂Sb₂Te₅ (GST) is one of the most commonly used PCMs in silicon-based optical switches due to its significant refractive index contrast ($\Delta n \approx$ 2. 8 at 1550 nm) between crystalline and amorphous states [11-15]. However, the imaginary part of the refractive index of GST is large, which is 1.08 and 0.12 at crystalline and amorphous states at 1550 nm^[9], respectively. This will introduce high loss in the MZI optical switch and limit its applications. Amorphous (Am-) and crystalline (Cr-) Sb₂Se₃ both have low extinction coefficients and exhibit large optical contrast ($\Delta n \approx$ 0.77 at 1550 nm) in the near infrared wavelength range, making it highly promising for applications in optical switches^[16]. In this work, we proposed a broadband high-extinction-ratio 2×2 MZI nonvolatile optical switch based on Sb₂Se₃. The introduction of a $\pi/2$ pre-biased waveguide structure reduces the required

length of $\mathrm{Sb_2Se_3}$ to change the ON/OFF state of the switch, which reduces the absorption loss of crystal-line $\mathrm{Sb_2Se_3}$ and lowers the power consumption for phase transition of $\mathrm{Sb_2Se_3}$. The loss is 0. 84 dB at the wavelength of 1550 nm for both bar and cross states. The power consumption is 105. 86 nJ and 49 nJ for crystallization and amorphization of $\mathrm{Sb_2Se_3}$, respectively. The symmetric integration of $\mathrm{Sb_2Se_3}$ in both phase-shift arms improves the extinction ratio (ER). The ER reaches 28. 8 dB at the wavelength of 1550 nm. The proposed 2×2 MZI nonvolatile optical switch also has a wide bandwidth of greater than 150 nm.

1 Design of device

The designed 2×2 MZI nonvolatile optical switch based on low-loss Sb₂Se₃ consists of two 2×2 multimode interferometers (MMIs) and phase-shift arms, as shown in Fig. 1(a). To reduce the crosstalk at the MMI output, curved waveguides with radius of 10 µm were used to connect MMIs and phase-shift arms. MMI has the advantages of wide bandwidth and large fabrication tolerance. Two 2×2 MMIs are used as power splitter and combiner, respectively. The phase shifters are composed of Si-Sb₂Se₃ hybrid waveguides (Fig. 1 (b)). When only one phase-shift arm integrates phase-change material, the large loss difference between the upper and lower phase-shift arms will reduce ER, especially in Cr-Sb₂Se₃. Thus, to improve ER, Sb₂Se₃ is integrated in both the upper and lower phase-shift arms. To shorten the length of



: Fig. 1. (a) Schematic diagram of the proposed 2×2 MZI nonvolatile optical switch. (b) Cross-section of the Si-Sb₂Se₃ hybrid waveguide with the ITO heater. (c) Schematic diagram of the π/2 pre-biased waveguide structure :图 1. (a) 2×2 MZI 型非易失性光开关结构示意图。(b) 带有 ITO 加热器的 Si-Sb₂Se₃ 混合波导截面图。(c) π/2 预偏置波导结构示意图

Sb₂Se₃, which can reduce the absorption loss especially of crystalline Sb₂Se₃ and lower the power consumption for phase transition of Sb₂Se₃, we introduced a $\pi/2$ pre-biased waveguide structure in the lower phaseshift arm $^{[17]}$. In this way, only a $\pi/2$ phase shift needs to be achieved by the phase transition of Sb₂Se₂ to control the ON/OFF state of the switch. Through the $\pi/2$ pre-biased structure has been reported in reference [17], it works at the wavelength of 2 μm. We designed and optimized the $\pi/2$ pre-biased structure at the wavelength of 1550 nm, and firstly introduced it in the Sb_2Se_3 optical switch. The $\pi/2$ pre-biased structure contains two symmetric tapered waveguide whose width transits from w = 500 nm to $w_2 = 544$ nm with a total length L of 12 μ m (Fig. 1(c)). Then, the Si-Sb₂Se₃ hybrid waveguide was optimized by the finite element method (FEM). Considering compatibility with the complementary metal-oxide-semiconductor (CMOS) fabrication process and single-mode condition, we determined the silicon waveguide dimensions to be 220 nm in thickness and 500 nm in width. At the wavelength of 1550 nm, the refractive index of Si and SiO_2 is 3. 476 + iO_3 , 1. 444 + iO_3 , respectively^[18, 19]. We fabricated layered Sb₂Se₃ and measured its optical constants at amorphous and crystalline states by ellipsometer, as shown in Fig. 2. The measurement results indicate that the refractive index of amorphous and crystalline Sb₂Se₃ is 3. 321 + i0 and 4. 024 + i0. 0087 at the wavelength of 1550 nm, respectively. The change of effective refractive index difference (Δn_{eff}) of transverse electric (TE) mode in the Si-Sb₂Se₃ hybrid waveguide at the amorphous and crystalline states with the size of Sb₂Se₃ is shown in Fig. 3(a). Clearly, $\Delta n_{\rm eff}$ increases along with the thickness h_1 of Sb₂Se₃, while firstly increases with the width w_1 of Sb₂Se₃ and then tends to be stable when $w_1 > 1 \mu m$. According to the phase calculation formula:

$$\Delta \varphi = \frac{2\pi \Delta n_{\text{eff}}}{\lambda} \times L, \tag{1}$$

the larger $\Delta n_{\rm eff}$, the shorter the required length of Sb₂Se₃ to achieve the desired phase shift. So, we determined the width w_1 of Sb₂Se₃ to be 1 μ m. At the wavelength of 1550 nm, the required length $L_{(\pi/2)}$ of Sb₂Se₃ to achieve $\pi/2$ phase shift at different size of Sb₂Se₃ is

shown in Fig. 3 (b). $L_{(\pi/2)}$ reduces as the thickness h_1 of Sb₂Se₃ increases. The absorption loss of the Si- $\mathrm{Sb}_{2}\mathrm{Se}_{3}$ hybrid waveguide can be calculated by $\alpha_{\mathrm{dB}}L_{(\pi/2)}$, where α_{dB} is the power propagation loss in dB/ μ m. α_{dB} can be converted from the propagation loss constant α (μm^{-1}) by the formula $\alpha_{\text{dB}} = 20\alpha / \ln 10 \text{ (dB/}\mu\text{m})^{[20]}$. According to $\alpha = 2\pi k_{\text{neff}}/\lambda$, so α_{dB} can be calculated by $\alpha_{dB} = 40\pi k_{neff} / (\lambda \ln 10) (dB/\mu m)$, where k_{neff} is the imaginary part of effective refractive index of the Si-Sb₂Se₂ hybrid waveguide at the crystalline state and is shown in Fig. 3(c). So, we can derive the absorption loss of the Si-Sb₂Se₃ hybrid waveguide at different thickness h_1 and width w_1 of Sb₂Se₃, as shown in Fig. 3 (d). The absorption loss increases slightly along with the thickness h_1 of Sb₂Se₃. However, Δn_{eff} increases along with h_1 , as mentioned above. Considering the thicker the PCM, the more difficult the phase transition and the greater the power consumption, the thickness h_1 of Sb₂Se₃ is chosen to be 50 nm.

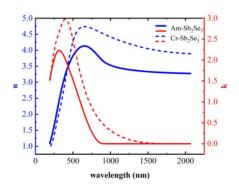


Fig. 2 Optical constants of layered Sb₂Se₃ at crystalline and amorphous states measured using ellipsometry in the experiment.
图 2 椭偏仪测量的 Sb2Se3 薄膜在晶态和非晶态下的光学

常数

The phase transition of Sb_2Se_3 is actuated by indium tin oxide (ITO) heater. ITO is compatible with CMOS process and its fabrication process is simple, making it more suitable for applications with large-scale integration of optical switches^[21,22]. The cross-section of the $Si-Sb_2Se_3$ hybrid waveguide with ITO heater ($Si-Sb_2Se_3$ -ITO waveguide) is shown in Fig. 1 (b). The introduction of the ITO heater will affect the optical mode, which will further change the required length of Sb_2Se_3 to achieve $\pi/2$ phase shift and absorp-

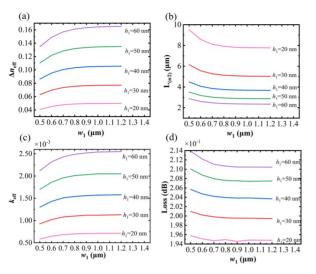


Fig. 3 Structural parameter optimization. (a) Effect of the size of Sb_2Se_3 on the difference of effective refractive index $(\Delta n_{\rm eff})$ of the $Si\text{-}Sb_2Se_3$ hybrid waveguide at the amorphous and crystalline states. (b) The required length of Sb_2Se_3 to achieve $\pi/2$ phase shift at different thickness and width of Sb_2Se_3 . Effect of the size of Sb_2Se_3 on the (c) imaginary part $(k_{\rm eff})$ of effective refractive index and (d) absorption loss of the $Si\text{-}Sb_2Se_3$ hybrid waveguide at the crystalline state. The optimization was implemented for TE mode at the wavelength of 1550 nm

图 3 结构参数优化。(a) Sb2Se3处于非晶态和晶态时 Si-Sb2Se3 混合波导有效折射率差 (Δ neff) 与 Sb2Se3 的厚度和宽度的变化关系。(b) 实现 π /2 相移所需的 Sb2Se3 长度与 Sb2Se3 的厚度和宽度的变化关系。Sb2Se3处于晶态时,Si-Sb2Se3 混合波导的(c) 有效折射率虚部(keff)和(d)吸收 损耗随 Sb2Se3 厚度和宽度的变化关系。以上结果是在 1550 nm 波长下基于 TE 模式得到的

tion loss at the crystalline state. We optimized the thickness h_2 of ITO by FEM. We fabricated the ITO film and measured its optical constant by ellipsometer, as shown in Fig. 4(a). The complex refractive index of ITO is $2.021 + i\ 0.0049$ at the wavelength of 1550nm. Similar to the optimization of the Si-Sb₂Se₃ hybrid waveguide, we can derive the required length of the $Si-Sb_2Se_3-ITO$ waveguide $(L'_{(\pi/2)})$ and the absorption loss of the Si-Sb₂Se₃-ITO waveguide in Cr-Sb₂Se₃according to the simulated effective complex refractive index and corresponding formulas, as shown in Fig. 4 (b). The required length reduces as h_2 increases, while the absorption loss increases. The shorter the Si- $\mathrm{Sb_2Se_3} ext{-ITO}$ waveguide $(L'_{\scriptscriptstyle(\pi/2)})$, the lower the power consumption for the phase transition of Sb₂Se₃ and the more beneficial to the miniaturization of the device. To balance the required length and absorption loss, the ITO thickness is chosen to be 30 nm. So only 2.71 μm long Sb₂Se₃ at the wavelength of 1550 nm is needed to realize $\pi/2$ phase shift (Fig. 4(b)). The simulated cross–section normalized mode profiles of TE mode in the Si–Sb₂Se₃–ITO waveguide in Cr–Sb₂Se₃ and Am–Sb₂Se₃ are shown in Fig. 4(c) and Fig. 4(d), respectively.

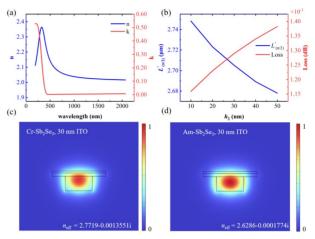


Fig. 4 (a) Optical constant of the fabricated ITO film measured by ellipsometry in the experiment. (b) Effect of ITO thickness on the required length of the Si-Sb₂Se₃-ITO waveguide to achieve $\pi/2$ phase shift and the absorption loss of the Si-Sb₂Se₃-ITO waveguide at the crystalline state of Sb₂Se₃. The cross-section normalized mode profiles of TE mode in the Si-Sb₂Se₃-ITO waveguide in (c) Cr-Sb₂Se₃ and (d) Am-Sb₂Se₃ when $h_1 = 50$ nm, $h_2 = 30$ nm and $w_1 = 1$ μ m. The simulation was implemented for TE mode at the wavelength of 1550 nm 图 4 (a) 使用椭偏仪测量的 ITO 薄膜的光学常数。(b) 实 现 π/2 相移对应的 Si-Sb2Se3-ITO 混合波导长度和 Sb2Se3 处于晶态时 Si-Sb2Se3-ITO 的吸收损耗随 ITO 厚度的变化关 系。当 h1 = 50 nm、h2 = 30 nm 和 w1 = 1 μm 时, Si-Sb2Se3-ITO 波导中(c) Sb2Se3 处于晶态和(d) Sb2Se3 处于非晶态 时 TE 模式的归一化模场分布图。以上结果是在 1550 nm 波 长下基于TE模式得到的

2 Results and discussions

2. 1 Optical Performance

We used the finite-difference time-domain (FDTD) method to study the optical performance of the proposed 2×2 MZI nonvolatile silicon-based optical switch. When Sb_2Se_3 in the lower and upper phase-shift arms are at the crystalline and amorphous states, respectively, the light outputs from the bar port, as shown in Fig. 5(a). The total IL is 0.84 dB and the ER reaches 28.8 dB at the wavelength of 1550 nm (Fig. 5(b)). Inversely, when Sb_2Se_3 in the lower and upper phase-shift arms are at the amorphous and crystalline states, respectively, the light outputs from the cross port (Fig. 5(c)) with an IL of 0.84 dB and an ER of 19.8 dB at the wavelength of 1550 nm (Fig. 5

(d)). The IL is mainly caused by two reasons. One is the absorption of crystalline Sb_2Se_3 and ITO, and the other is the mode mismatch between the Si waveguide and the $Si-Sb_2Se_3$ -ITO waveguide. The IL can be further reduced by introducing a coupler structure between the Si waveguide and the $Si-Sb_2Se_3$ -ITO waveguide or by designing micro-nano structured Sb_2Se_3 . As shown in Fig. 5(b), the 3 dB bandwidth of the optical switch is greater than 150 nm at bar state and the ER is greater than 20. 3 dB in the 3 dB bandwidth. At cross state, the 3 dB bandwidth is also greater than 150 nm and the ER is greater than 16. 3 dB in the 3 dB bandwidth (Fig. 5(d)).

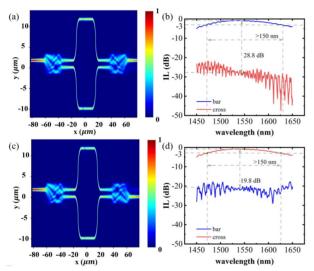


Fig. 5 The simulated electric field distribution diagram of the optical switch at (a) bar state and (c) cross state and the transmission at (b) bar state and (d) cross state 图 5 光开关在 (a) 直通态和 (c) 交叉态时的电场分布图,以及在 (b) 直通态和 (d) 交叉态下的透射谱

2. 2 Thermal Simulations

We implemented thermal simulation for the phase transition of Sb_2Se_3 . The resistivity of ITO is 1.6×10^{-3} $\Omega\cdot cm^{[24]}$. The material properties used in the thermal simulation are summarized in Table 1. The metal electrode is Au, as shown in Fig. 1(b). The distance from Au to the middle of the $Si-Sb_2Se_3$ -ITO waveguide is

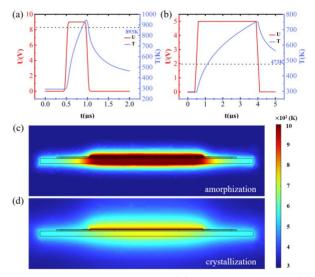


Fig. 6 Thermal simulation of (a) amorphization and (b) crystallization processes. Thermal distribution of the phase-shift arm along longitudinal section at the middle of waveguide for (c) amorphization and (d) crystallization processes 图 6 (a) 非晶化过程的热仿真;(b) 结晶过程的热仿真。在波导中部,相移臂沿纵向截面的热分布:(c) 非晶化过程;(d) 结晶过程

2. 1 µm to prevent metal absorption. For amorphization, Sb₂Se₃ must be rapidly heated to its melting point 893 K and then followed by quick cooling. Therefore, a high and short pulse with 9 V amplitude and 500 ns width is used, as shown by the red line in Fig. 6(a). As the blue line in Fig. 6(a) and Fig. 6(c) show, the temperature of the whole Sb₂Se₃ exceeds 893 K, suggesting Sb₂Se₃ realizes amorphization completely. The corresponding power consumption is about 49 nJ. For crystallization, the temperature of Sb₂Se₃ needs to be controlled between the crystal temperature 473 K and the melting point 893 K. A low and long pulse with 5 V amplitude and 3.5 µs width is used, as shown by the red line in Fig. 6 (b). Similarly, the whole Sb₂Se₃ realizes crystallization, as shown by the blue line in Fig. 6(b) and Fig. 6(d). The corresponding power consumption is about 105.86 nJ. The introduction of the $\pi/2$ pre-bias structure reduces the required length of Sb₂Se₃, which reduces the power consump-

Table 1 Physical parameters of materials used in the thermal simulation.

表 1 在热仿真中所用材料的物理参数

Materials	SiO_2	Si	$\rm Am\!-\!Sb_2\!Se_3$	$\mathrm{CrSb}_{2}\mathrm{Se}_{3}$	ITO
Density [kg/m³]	2203	2329	~6000	6500	$7100^{[23]}$
Thermal conductivity [$W/m \cdot K$]	1.38	130	0. 2	0. 24	~1340 ^[23]
Heat capacity at constant pression $[J/kg \cdot K]$	746	700	150	150	11[23]

tion for phase transition of Sb_2Se_3 . Additionally, the ITO heater we designed fully covers and contacts the Sb_2Se_3 , enhancing the heating efficiency and further minimizing the energy loss. Table 2 summarizes a comparison for the performance of the 2×2 nonvolatile optical switches in the literature with our work. Our 2×2 MZI nonvolatile optical switch exhibits outstanding characteristics in terms of PCMs length, bandwidth, ER and IL. Moreover, the IL can be further reduced by introducing a coupler structure between the Si waveguide and the $Si-Sb_2Se_3$ -ITO waveguide or by designing micro-nano structured Sb_2Se_3

3 Conclusions

We demonstrated a broadband high–extinction–ratio 2×2 MZI nonvolatile silicon–based optical switch based on phase change material $\mathrm{Sb}_2\mathrm{Se}_3$. By introducing a $\pi/2$ pre–biased waveguide structure, only 2.71 μm long $\mathrm{Sb}_2\mathrm{Se}_3$ is needed to tune the switch state, which reduces the absorption loss of crystalline $\mathrm{Sb}_2\mathrm{Se}_3$ and the power consumption for the phase transition of $\mathrm{Sb}_2\mathrm{Se}_3$. When $\mathrm{Sb}_2\mathrm{Se}_3$ in the lower and upper phase–shift arms are at crystalline and amorphous states, respectively, light outputs from the bar port. The IL is

0.84 dB and the ER reaches 28.8 dB at the wavelength of 1550 nm. Inversely, light outputs from the cross port with an IL of 0. 84 dB and an ER of 19. 8 dB at the wavelength of 1550 nm. At both states, the 3 dB bandwidth is greater than 150 nm. The ER is greater than 20.3 dB and 16.3 dB at bar and cross states in the 3 dB bandwidth, respectively. We used a low and long pulse with 5 V amplitude and 3.5 µs width to achieve the crystallization and a high and short pulse (9 V amplitude, 500 ns width) for amorphization. The corresponding power consumption is 105.86 nJ and 49 nJ, respectively. To the best of our knowledge, we have achieved an excellent 2×2 MZI nonvolatile optical switch, which is better than other 2×2 nonvolatile optical switches especially in terms of bandwidth, ER, and IL. Because of the superior characteristics, our optical switch holds considerable potential in the field of optical interconnects and optical comput-

Table 2 Comparison of the reported 2×2 nonvolatile optical switches with our work. 表 2 此工作与已报道的 2×2 非易失性光开关的比较

	Structure	PCM	PCMs Length	IL(@1550 nm)	BW^1	ER	Phase transition approach	Power	S/E ²	
Jiang ^[25]	$3W^3$ DC ⁴	GSST ⁵	12 μm	Bar: 1. 14 dB Cross: 0. 38 dB	100	Bar: >12. 3 dB	/	/	S	
Song ^[26]	Song ^[26] MSW ⁶ Sb	ch c	0.4	Bar; 0. 073 dB Cross; 0. 055 dB	nm 35	Cross: >10. 27 dB Bar: >13. 6 dB	PIN heat-	1	S	
Song MSW	Sb_2S_3	9. 4 μm	Dar: U. U/3 ad Gross: U. U33 ad	nm	Cross: $>15.3~\mathrm{dB}$	er	/	3		
Yang ^[27]				Bar: 1. 69 dB Cross: 2. 93 1543. 85 nm	dB @	≈10 nm	Bar: >10 dB Cross: >10 dB	RTA ⁷	/	Е
		MZI	Sb_2S_3 3. 8	8 μm Bar: 0. 6 dB Cross: 0. 6	dB	≈40 nm	Bar: >20 dB Cross: >20 dB	/	/	s
Yang ^[28]	MZI	MZI Sb ₂ Se ₃ 18 μm	Bar; 2. 5 dB Cross; 2. 5 dB	60	Bar: >20 dB	PIN heat-	≈1 µJ /	Е		
Li ^[29]	MZI/DC	$\mathrm{Sb_2Se_3}$	1. 63 μm	Bar; 0. 068 dB Cross; 0. 034 dB	nm 64 nm	Cross: >20 dB Bar: >15 dB Cross: >15 dB	er /	≈100 nJ /	S	
Shang ^[30]	MMI	$\mathrm{Sb_2Se_3}$	~27 µm	Bar; 1. 16 dB Cross; 0. 66 dB @ 1570 nm	35 nm	Bar: >15 dB Cross: >15 dB	RTA	/	E	
This work	MZI	$\mathrm{Sb_2Se_3}$	2.71 μm	Bar: 0. 84 dB Cross: 0. 84 dB	150 nm	Bar: >20. 3 dB Cross 16. 3 dB	er ITO heat-	105. 86 nJ / 49 nJ	s	

¹BW: Bandwidth, ²S/E: Simulation/Experiment, ³3W: 3 Waveguide, ⁴DC: Directional coupler, ⁵GSST: Ge₂Sb₂Se₄Te₁, ⁶MSW: Multimode slot waveguide, ⁷RTA: Rapid thermal annealing.

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