

一维光子准晶平 V 透镜

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摘要: 一维光子准晶已在亚波长、亚衍射聚焦及超分辨成像领域不断展现优越性。为丰富及拓展其聚焦特性的应用, 本文提出了一种一维光子准晶平 V 透镜, 并研究了材料厚度对其聚焦特性的影响。研究结果表明, 该透镜可在第二能带较宽的波长范围内实现亚波长及亚衍射聚焦。本文研究结果将为一维光子准晶平 V 透镜的设计及应用提供参考。

关 键 词: 光子准晶; 透镜; 亚波长聚焦; 亚衍射聚焦

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One-dimensional photonic quasi-crystal plano-V lens

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Abstract: One-dimensional photonic quasi-crystal (1D PQC) has continuously shown their superiority in the fields of sub-wavelength focusing, sub-diffraction focusing and super-resolution imaging. In order to enrich and expand the application of its focusing characteristics, a 1D PQC plano-V lens is proposed and the effect of material thickness on its focusing characteristics is studied in this paper. The results show that the lens can achieve sub-wavelength focusing and sub-diffraction focusing in a wide wavelength range of the second band. The results in this paper will provide reference for the design and application of 1D PQC plano-V lens.

Key words: photonic quasi-crystal, lens, sub-wavelength focusing, sub-diffraction focusing

引言

随着集成光学及微纳光子学的不断发展^[1-11], 微透镜与微透镜阵列^[12-15]因其体积小、重量轻、便于集成化及阵列化等优点而成为研究热点。光子晶体透镜作为微透镜的杰出代表之一, 在亚波长、亚衍射聚焦及超分辨率成像方面具有良好的性能^[16-20], 且准周期光子晶体(又称为光子准晶)透镜的聚焦及成像特性^[21-27]优于周期光子晶体透镜。

光子准晶因具有特殊的结构特征(如:二维光子准晶具有长程有序性、旋转对称性、自相似性^[28-30]; 一维光子准晶具有 Fibonacci 序列^[31-33]、Thue-Morse 序列结构^[34-36])而使其散射子具有多种

位置特征。因此, 与周期光子晶体^[37-38]相比, 光子准晶在设计过程中可调节的参数更多, 且可实现广泛应用, 如: 透镜^[21-27]、光纤^[39-47]、棱镜^[48]、滤波器^[39,49-50]、传感器^[43,46,51-52]、空芯光束的产生^[53]及拓扑光子器件^[54]等。目前, 光子准晶透镜亚波长、亚衍射聚焦及超分辨成像的研究主要集中于二维光子准晶^[21-24,27], 而一维光子准晶透镜的研究则相对薄弱。相对于二维光子准晶结构, 一维光子准晶结构更简单, 在制作上也相对容易, 便于推广应用。另外, 与当前研究较多的超表面平面透镜^[55-56]相比, 一维光子准晶透镜也具有一定优势。超表面平面透镜一般是二维结构, 制备较复杂, 且其周期结构使得制备误差对光学性能影响较大, 而一维光子准晶

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透镜则可避免这些问题。虽我们已开展了一维光子准晶的聚焦特性研究,但仅限于平凹透镜^[25-26]及圆形光栅^[57]。为丰富及拓展一维光子准晶聚焦特性的应用,其它结构的一维光子准晶透镜尚待研究。

本文提出了一种V形Fibonacci光子准晶透镜,分析了聚焦特性随电介质厚度变化的规律。

1 模型与算法

传统光学透镜的分辨率受Rayleigh衍射极限的限制。倏逝波在穿过传统光学透镜后呈指数衰减而不能到达成像面参与成像,其携带的物方信息被丢失。光子晶体作为一种人工微结构材料,其在第二通带可实现负折射,从而增强倏逝波的振幅,修复倏逝波的相位,提高透镜的分辨率^[16-20],从而实现亚波长聚焦。类比周期光子晶体,光子准晶在第二通带也会发生负折射^[25-26]。这种具有传播和增强倏逝波性能的透镜可提高成像分辨率及聚焦效果。

在数学上,Fibonacci序列是指:1、1、2、3、5、8、13、21、34、……。在形式上,Fibonacci序列可用递推的形式定义: $F(0)=0, F(1)=1, F(2)=1, F(m)=F(m-1)+F(m-2)$ ($m \geq 2, m \in \mathbb{N}$)^[58]。若把两种不同介质材料(设为A、B)按Fibonacci序列排布即可构成Fibonacci光子准晶。如图1(a),若m取不同的数值,则可得到不同的Fibonacci光子准晶。设 $F(0)=B, F(1)=A$,则 $F(2)=F(1)+F(0)=AB, F(3)=F(2)+F(1)=ABA, F(4)=F(3)+F(2)=ABAAB$ ……。根据现实功能需要,取不同材料、厚度、层数及外形结构与尺寸,可设计不同的Fibonacci光子准晶器件(如本文设计的一维光子准晶平V透镜,如图1(b))。

如图1(a),设电介质材料A、B分别为 SiO_2 、Ge,其折射率分别为 $n_A=1.56, n_B=4.00$,其厚度分别为 d_A, d_B 。透镜的横截面,如图1(b)所示,其宽度、高度、V形平台宽度及底座高度分别设为 L, h, L_1, h_1 。V形坡面采用光栅结构。平面光波从透镜底部入射,并汇聚于透镜上方。设焦点半宽度(full width at half maximum)FWHM= $\eta\lambda$,系数 η 值越小,其焦点质量越好。

为了研究透镜的聚焦特性,首先需分析透镜的光子能带结构,以得到可在透镜中传输的波长范围。因光子准晶不具有周期结构(平移对称性),故其能带结构不可用色散关系表征,本文采用透射谱表征其能带结构。通过传输矩阵法,首先计算光子准晶的透射系数^[59]。对于TE模式,由于介质A的厚

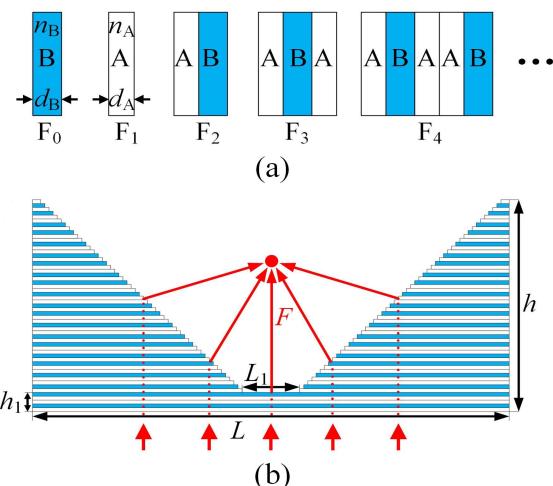


图1 (a) 具有Fibonacci序列的结构示意图 (b) Fibonacci光子准晶平V透镜的二维模型,红色箭头表示平面波的入射方向及穿过透镜后汇聚到焦点的过程,F为透镜的焦距

Fig. 1 (a) Structure diagram with the Fibonacci sequence (b) 2D model of the Fibonacci photonic quasi-crystals (PQC) plano-V lens. The red arrows indicate the incident direction of the plane wave and the process of converging to the focal point after passing through the lens. F is the focal distance of the lens

度为 $d_A=100\text{nm}$ 不变,其传输矩阵 M_A 可由下式表示:

$$M_A = \begin{bmatrix} \cos\delta_A & \frac{i}{\eta_A} \sin\delta_A \\ i\eta_A \sin\delta_A & \cos\delta_A \end{bmatrix}. \quad (1)$$

介质B的厚度在 $d_B \in [10\text{nm}, 300\text{nm}]$ 范围内变化,所以其传输矩阵 M_{Bj} ($j \in [10, 300]$,步长 $\Delta j=5$,不同的j值对应不同厚度下的介质B)可由下式表示:

$$M_{Bj} = \begin{bmatrix} \cos\delta_{Bj} & \frac{i}{\eta_{Bj}} \sin\delta_{Bj} \\ i\eta_{Bj} \sin\delta_{Bj} & \cos\delta_{Bj} \end{bmatrix}, \quad (2)$$

其中

$$\delta_k = \frac{-2\pi}{\lambda} n_k d_k \cos\theta_i (k = A, B_j), \quad (3)$$

$$\eta_k = \sqrt{\frac{\epsilon_0}{\mu_0}} n_k \cos\theta_i (k = A, B_j), \quad (4)$$

其中 $\delta_k, \eta_k, d_k, \lambda, n_k, \epsilon_0$ 和 μ_0 分别是相位差、有效光导纳、电介质厚度、真空波长、电介质折射率、真空介电常数和磁导率。

当入射平面波穿过 N 层介质后,透射系数可表示为:

$$t = \frac{2\eta_0}{A\eta_0 + B\eta_0\eta_N + 1 + C + D\eta_N + 1}, \quad (5)$$

透射率可表示为:

$$T = t^2. \quad (6)$$

对于TM模式,表达式(5)和(6)同样适用,表达式(4)需要改为:

$$\eta_k = \sqrt{\frac{\epsilon_0}{\mu_0}} n_k / \cos\theta_t \quad (k = A, B_j). \quad (7)$$

由于本文中入射平面波均为垂直入射,折射角 θ_t 均为0,即TE模式下和TM模式下的透射率 T 相等,即本文提出的一维光子准晶平V透镜,入射平面光波的偏振方向并不影响透镜的聚焦效果。通过上述方法,可计算得到透镜($d_A=d_B=100\text{nm}$)的透射谱,如图2所示。

由图2可知,Fibonacci序列的光子准晶可产生

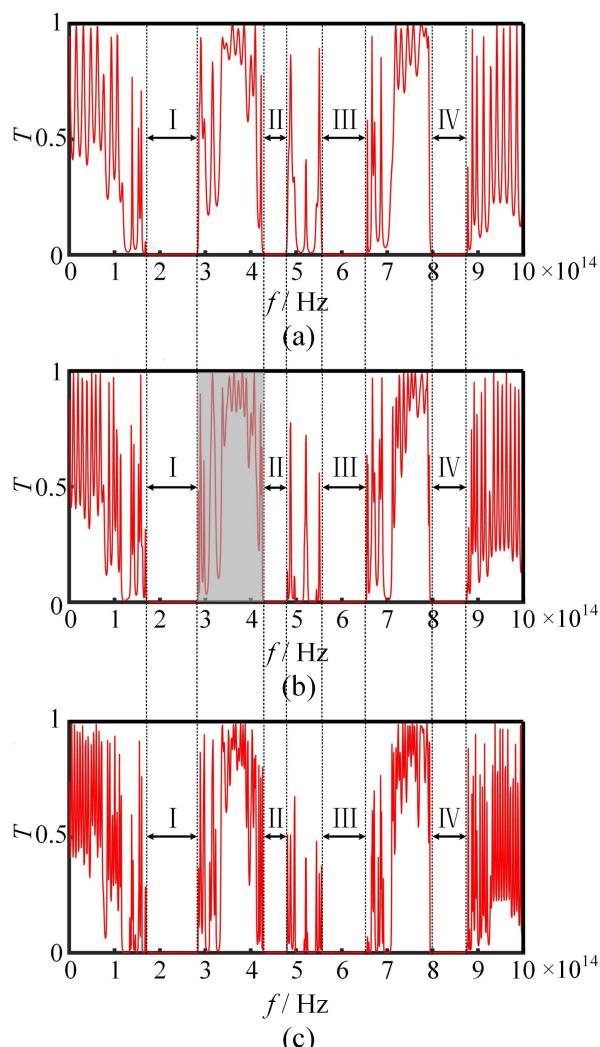


图2 具有不同Fibonacci序列的光子准晶的透射谱:(a) F(8) (b) F(9) (c) F(10)

Fig. 2 Transmission spectrum of a PQC with different Fibonacci sequences: (a) F(8) (b) F(9) (c) F(10)

四大带隙(见区域:I、II、III、IV),其所在的频率范围分别为 $f_I \in [1.717 \times 10^{14} \text{Hz}, 2.832 \times 10^{14} \text{Hz}]$, $f_{II} \in [2.832 \times 10^{14} \text{Hz}, 4.293 \times 10^{14} \text{Hz}]$, $f_{III} \in [4.293 \times 10^{14} \text{Hz}, 6.542 \times 10^{14} \text{Hz}]$, $f_{IV} \in [6.542 \times 10^{14} \text{Hz}, 7.961 \times 10^{14} \text{Hz}]$ 。F(8)中各带隙边缘存在些许弯曲,即带隙尚未完全成形。F(9)中各带隙边缘无弯曲,即带隙已完全成形。随着光子准晶层数的进一步增加,F(10)中各带隙边缘无弯曲,虽带隙保持稳定,但相对于F(9),其层数增加接近1倍,导致制备成本及难度大幅度增加。因此,选用F(9)作为透镜的序列数,既能达到较好的聚焦效果,又能节省材料且方便制备。

本文采用有限元法计算分析Fibonacci光子准晶平V透镜的聚焦特性。

2 结果与讨论

进一步仿真计算发现,在F(9)序列光子准晶的第二通带频段(见图2(b)灰色区域, $f_{\text{focus}} \in [2.832 \times 10^{14} \text{Hz}, 4.293 \times 10^{14} \text{Hz}]$ (此时 $d_B=100\text{ nm}$))可发生聚焦。不过,实际制备误差将导致聚焦频率发生偏离。为此,改变 $d_B \in [50 \text{ nm}, 200 \text{ nm}]$,可计算得到透镜对入射平面波的公共聚焦波段范围。以 $d_B=50\text{nm}$ 、 100nm 、 200nm 为例,透射光谱如图3所示。

当 d_B 取不同值时,透镜对入射平面波的聚焦频率范围如下:当 $d_B=50\text{ nm}$ 时, $f \in [3.139 \times 10^{14} \text{Hz}, 4.858 \times 10^{14} \text{Hz}]$;当 $d_B=100\text{ nm}$ 时, $f \in [2.832 \times 10^{14} \text{Hz}, 4.293 \times 10^{14} \text{Hz}]$;当 $d_B=200\text{ nm}$ 时, $f \in [2.742 \times 10^{14} \text{Hz}, 4.135 \times 10^{14} \text{Hz}]$ 。因此,公共聚焦频率范围为 $f_{\text{focus}} \in [3.139 \times 10^{14} \text{Hz}, 4.135 \times 10^{14} \text{Hz}]$ (见图3灰色区域)。从该频段中取平面波 $f=3.989 \times 10^{14} \text{Hz}$ (对应波长 $\lambda=752\text{ nm}$),研究材料厚度变化对透镜聚焦特性的影响。固定材料 SiO_2 的厚度 $d_A=100\text{ nm}$,且以 $\Delta d_B=5\text{ nm}$ 为间隔改变材料Ge的厚度 $d_B \in [10 \text{ nm}, 300\text{nm}]$,焦点的归一化焦点强度、FWHM系数 η 及焦距随 d_B 变化的规律,如图4所示。

由图4可知,随着 d_B 的增加,焦点的归一化焦点强度、FWHM系数 η 及焦距均呈振荡趋势。由图(a)可知,在 $d_B=10\text{ nm}, 100\text{ nm}, 185\text{ nm}, 265\text{ nm}, 275\text{ nm}$ 时,焦点强度取得局部最大值。由图(b)可知,当 $d_B \in [20 \text{ nm}, 65 \text{ nm}]$ 时, $0.5\lambda < \text{FWHM} < \lambda$,透镜实现了亚波长聚焦,而其它情况下, $\text{FWHM} > 0.5\lambda$,突破了衍射极限,也即透镜实现了亚衍射聚焦。由图(c)可知,当 $d_B=80\text{nm}, 185\text{nm}$ 时,焦距取得局部最大值。综合图4可知,当 $d_A=d_B=100\text{nm}$ 时,焦点强度最

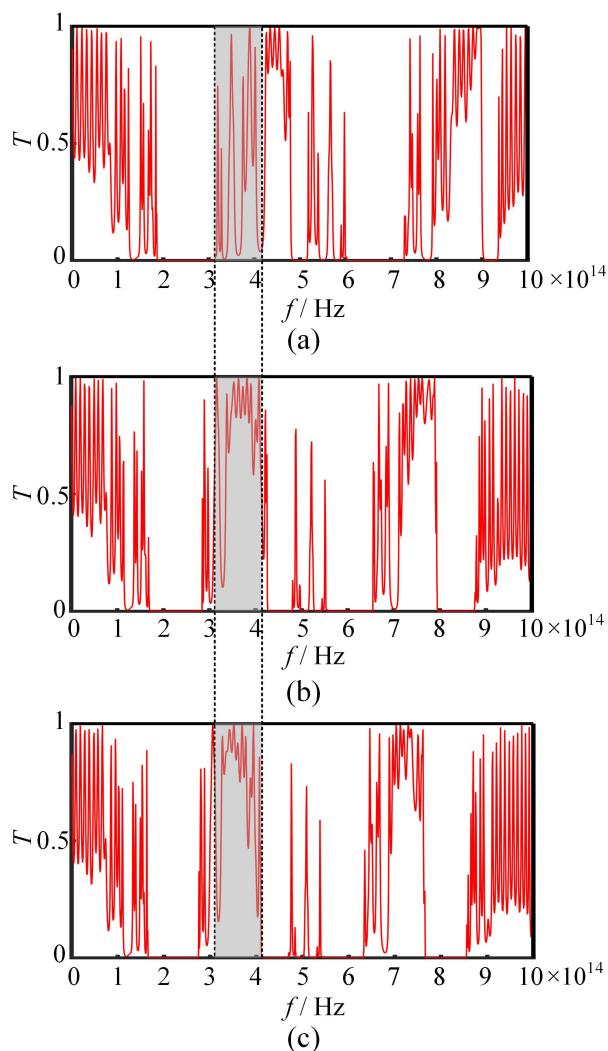


图3 $d_A=100\text{nm}$, d_B 变化时 Fibonacci 光子准晶的透射谱:(a) $d_B=50\text{nm}$ (b) $d_B=100\text{nm}$ (c) $d_B=200\text{nm}$

Fig. 3 Transmission spectrum of a PQC when $d_A=100\text{ nm}$ and d_B changes: (a) $d_B=50\text{ nm}$ (b) $d_B=100\text{nm}$ (c) $d_B=200\text{ nm}$

大,且 $\text{FWHM}=0.367\lambda$ 趋于最小,实现了最佳的亚衍射聚焦特性,如图5所示。

由图5可知,一维光子准晶平V透镜的聚焦点低于V形高度,使该透镜在超导纳米线单光子探测领域具有重要的潜在应用。超导纳米线单光子探测器的探测效率与纳米线对光子的吸收率密切相关,提高纳米线对光子的吸收率即可提高探测器的探测效率^[60]。若将超导纳米线单光子探测器的纳米线直接制作在透镜的V形凹槽内部,使纳米线置于透镜焦点处,则大部分的光子汇集于纳米线上,从而可大幅提升探测器的探测效率。另外,相较于一维光子准晶平凹透镜^[25-26],本文提出的一维光子准晶平V透镜最佳焦点的半高宽FWHM更小,焦点

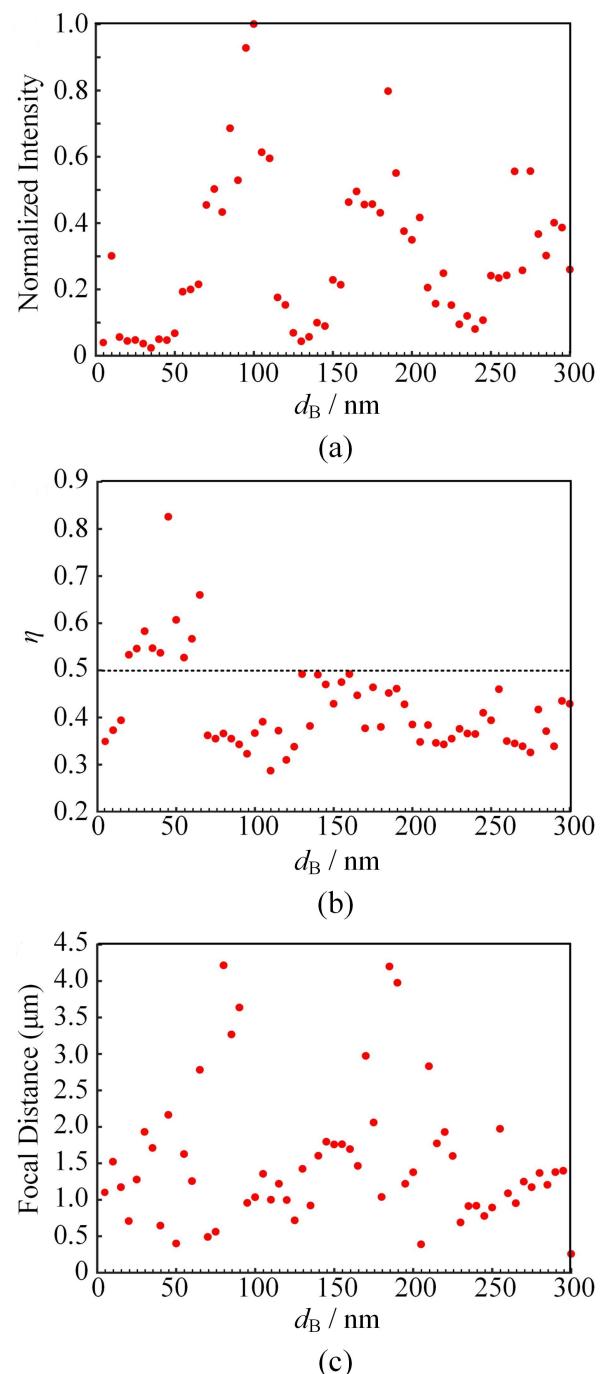


图4 Fibonacci 光子准晶平 V 透镜在 $\lambda=752\text{nm}$ 且 d_B 变化时的聚焦特性:(a)归一化焦点强度 (b)FWHM 系数 η ; (c)焦距

Fig. 4 The focusing characteristics of Fibonacci PQC plano-V lens when $\lambda=752\text{nm}$ and d_B varies: (a) normalized intensity of focus, (b) FWHM coefficient η , and (c) focal distance

旁瓣更小,且该透镜可调参数更多,这意味着可以更加细微地去调节透镜结构,从而实现更好的亚波长、亚衍射聚焦效果。

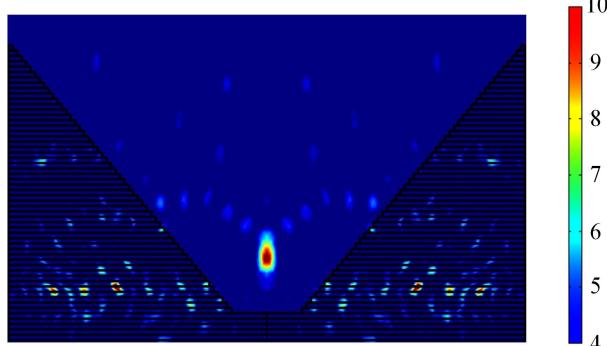


图5 $d_A=d_B=100$ nm的Fibonacci光子准晶平V透镜对平面波 $\lambda=752$ nm的聚焦场

Fig. 5 Focusing field of the Fibonacci PQC plano-V lens with $d_A=d_B=100$ nm for a plane wave $\lambda=752$ nm

3 结论

提出了一种Fibonacci序列光子准晶平V透镜，并分析了透镜随电介质材料厚度变化的亚波长、亚衍射聚焦特性。该透镜可以在一个较宽波长范围内实现亚波长、亚衍射聚焦。研究结果可为一维光子准晶平V透镜的材料选择、结构设计及应用提供参考。

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