

Three-dimensional structure analysis of Schottky barrier diode in CMOS technology for terahertz imaging

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Abstract: A simple and effective design method for high cut-off frequency Schottky barrier diode is proposed and implemented. The cut-off frequency of the processed Schottky barrier diode is about 800 GHz, which can reach about 1 THz with the optimized parameters through the test results and simulation data in SMIC 180 nm process. The integrated detector including antennas, matching circuit and Schottky barrier diode is completed, whose tested responsivity could achieve 130 V/W and noise equivalent power is estimated to be $400 \text{ pW}/\sqrt{\text{Hz}}$ at 220 GHz. The imaging experiment of invisible liquid surface in ceramic bottles has been completed and good results have been achieved.

Key words: complementary metal oxide semiconductor (CMOS), detector, imaging, Schottky barrier diode, terahertz

PACS: 07. 57. Kp

用于太赫兹成像的 CMOS 肖特基二极管三维结构研究

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摘要: 提出了一种简单、科学、有效的高截止频率肖特基势垒二极管设计方法。通过 SMIC 180 nm 工艺制备的肖特基二极管的截止频率为 800 GHz, 分析测试结果和仿真数据优化后的肖特基势垒二极管截止频率可以达到 1 THz 左右。完成了包括天线、匹配电路和肖特基势垒二极管的集成探测器, 在 220 GHz 下其测试响应率可达 130 V/W, 等效噪声功率估计为 $400 \text{ pW}/\sqrt{\text{Hz}}$ 。完成了陶瓷瓶内不可见液面的成像实验并取得了良好的效果。

关键词: 互补金属氧化物半导体; 检波器; 成像; 肖特基二极管; 太赫兹 (THz)

中图分类号: TN454

文献标识码: A

Introduction

Lately, focus on terahertz (THz) technology has been growing rapidly owing to its great potential in the fields of imaging, medical, communication, astronomy, etc. [1-2]. A number of studies have been reported on THz imaging system, which is closer than spectroscopy to being commercialized in the near future [3]. complementary metal oxide semiconductor (CMOS) technology attracts high attention in THz imaging field with its low cost and high integration, which meets the needs of THz large-scale imaging array [4].

Two major THz detectors in the CMOS field have been extensively studied, field-effect transistor (FET)

detectors based on plasma-wave detection theory and Schottky barrier diode (SBD) detector based on square law detector theory [5-6]. Compared with FET detectors, SBD detectors have obvious advantages in responsivity, which is extremely important for THz imaging owing to the inherent high spatial loss of THz wave [7-8]. Since V. Milanovic and Sankaran successively realize Schottky contact in CMOS process by metallizing the contact on the n-well and contacting the metal silicide with the substrate, many related studies have been done on CMOS SBD [9]. Nevertheless, there is no SBD applicable to THz band in the existing standard CMOS library, which is a hot point and difficulty in the THz study field.

The CMOS technology-based THz detectors with dif-

Received date: 2020- 06- 29, revised date: 2020- 12- 25

收稿日期: 2020- 06- 29, 修回日期: 2020- 12- 25

Foundation items: Supported by National Natural Science Foundation of China (61527805)

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ferent detection mechanisms including plasma modes and Schottky barrier diodes have very high requirements for cut-off frequency. The cut-off frequency of SBD is closely related to the minimum size that CMOS technology can achieve. Many high cut-off frequency detectors come to the fore with the progress of technology. For example, a 0.86-THz 4×4 array CMOS technology-based SBD imager is reported with raster scan measurement^[10-11], and a 1×240 array compound InGaAs SBD imager is demonstrated as a real-time 1-D line scanner^[12].

The progress of technology has brought a great leap forward to the overall index of SBD detectors, but the influence of design factors on the index of detectors under the same technology can not be underestimated. There are two main ways to realize Schottky barrier diode in CMOS standard process: shallow trench isolation technology and Polysilicon gate separation technology, shown in Fig. 1. Polysilicon gate separation SBD has less interference to current path, less channel impedance and higher cut-off frequency, which means that it has greater potential in THz imaging field^[13].

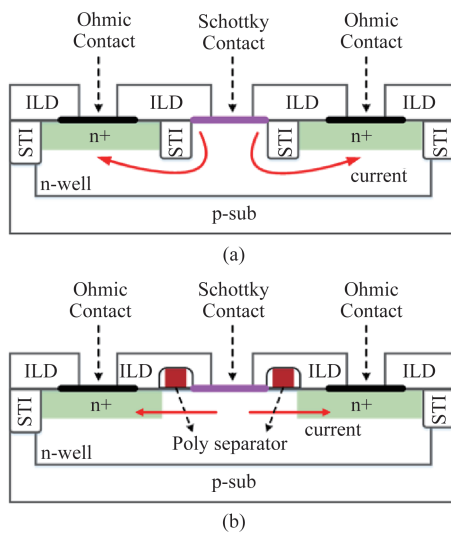


Fig. 1 Structure of two kinds of SBDs (a) shallow trench isolation SBD, (b) polysilicon gate separation SBD
图1 两种肖特基二极管结构 (a) 浅沟道隔离肖特基二极管, (b) 多晶硅栅隔离肖特基二极管

In this paper, we design a high-performance terahertz detector based on self-designed SBD in 180-nm CMOS foundry technology. In Sect. I, the three-dimensional structure of the polysilicon gate separation SBD is built, and the main factors affecting the cut-off frequency of Schottky barrier diode is analyzed and simulated. In Sect. II, we verify and optimize the data according to the results of the tape-out, and find out the technical points of designing a high cut-off frequency diode under the standard CMOS process. In Sect. III, we design a detector with a high-gain on-chip antenna and the key circuit architecture. Then, the terahertz imaging platform is built and the imaging experiment of liquid level detection in wine bottle is completed.

1 Structure analysis of Schottky barrier diodes

The three-dimensional structure of the diode is analyzed in detail to find the design method of high cut-off frequency diodes under the technological limitation, that is particularly important to terahertz detectors. The performance of polysilicon gate separation SBD is better than that of shallow trench isolation SBD in cut-off frequency, which determines our next major analysis of polysilicon gate separation SBD.

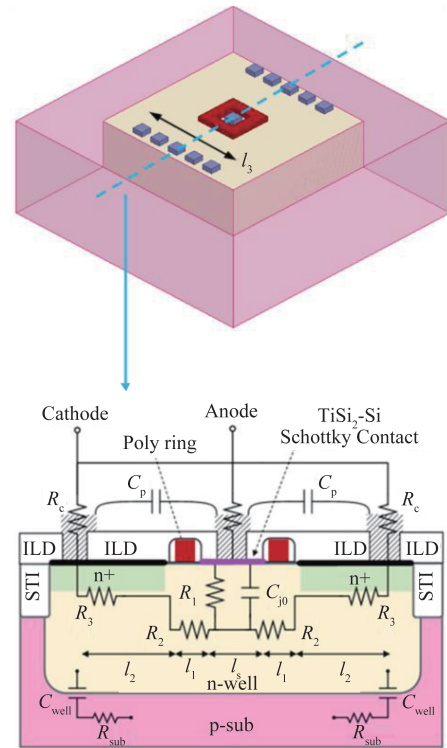


Fig. 2 The three-dimensional structure and two-dimensional profile of polysilicon gate separation SBD
图2 多晶硅栅隔离肖特基二极管的三维和二维结构示意图

As shown in Fig. 2, the polysilicon gate separation SBD separates Schottky contact between metal and lightly doped N-well and Ohmic contact between metal and heavily doped N-well by polysilicon ring.

Zero-bias cut-off frequency of SBD:

$$f_{co} = \frac{1}{2\pi R_s C_0} \quad , \quad (1)$$

R_s is series resistance and C_0 is diode capacitance at zero bias. The expressions of R_s and C_0 are derived as below. Individual components contributing to R_s and C_0 are shown in Fig. 2.

$$R_s \approx R_1 + R_2 + R_3 + R_c \quad , \quad (2)$$

$$R_s \approx R_v + \frac{R_{nwell}}{28.6} + R_{poly} \left(\frac{l_1}{4l_s} \right) + R_{n+} \left(\frac{l_2}{4(l_s + 2l_1)} \right) + R_c \quad (3)$$

$$C_0 = l_s^2 \sqrt{\frac{qN_D \epsilon_{Si}}{2\phi_B}} + C_p \quad , \quad (4)$$

where, R_v is the vertical component of R_1 , R_{nwell} is n-well sheet resistance, R_{poly} is the n-well sheet resistance under the poly separation ring, $R_{\text{n+}}$ is salicide n+ sheet resistance, R_c is the overall resistance of vias and contacts, N_D is n-well doping density, ϵ_{Si} is the permittivity of silicon, Φ_B is the built-in potential, and C_p is the parasitic capacitance of metal terminals. The factor of $1/28.6$ is derived from the base-spreading resistance model in Ref. [14]. In addition, l_s is the side length of square Schottky contact, l_1 is the width of polysilicon ring, l_2 is the length of polysilicon to cathode metal contact. The coefficients $1/4$ and $1/2$ in Eq. 3 correspond to the parallel calculation of 4 polysilicon ring and 2 cathode metal in the diode structure diagram, respectively.

From the above analysis, we can get that l_s is approximately inversely proportional to the cut-off frequency, that is, smaller anode contact area can get higher cut-off frequency, which is described in many articles. Owing to the obvious limitation of technology on l_s and l_1 , our main research objectives are l_2 and l_3 , which only affects a part of the total resistance and capacitance. And their changes have the opposite effect on the resistance and capacitance values, that requires us to reverse design according to the actual results.

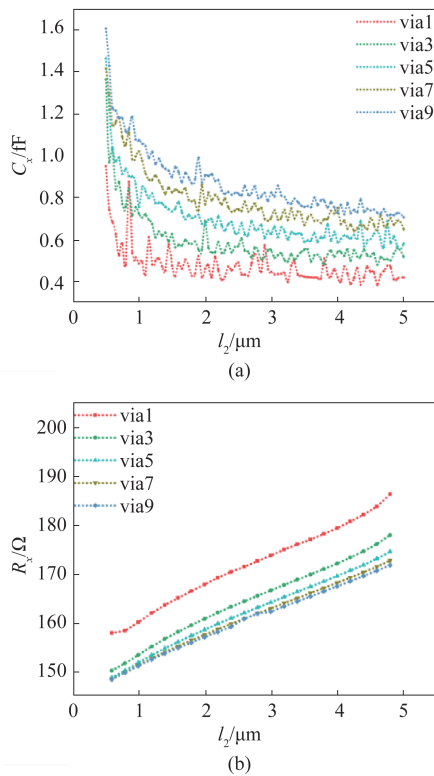


Fig. 3 Simulation result of the effect of l_2 and l_3 on resistance and capacitance (a) capacitance curve, (b) resistance curve
图3 l_2 和 l_3 对电阻电容的影响分析 (a) 电容曲线, (b) 电阻曲线

The simulation results of l_2 and l_3 using Sentaurus and HFSS software with fixed N-well size are shown as Fig. 3. R_x and C_x respectively represent the total resis-

tance and the parasitic capacitance C_p between the positive electrodes and negative electrodes. The length of l_3 determined by the number of vias in the negative electrode cannot be continuously changing due to process limitation. In Fig. 3, via X indicates that the negative electrode consists of X vias. As we can see from Fig. 3, with the increase of l_2 , the resistance will increase and the capacitance will decrease, while l_3 has the opposite effect. It is important to observe that this change is not linear, which shows that the effect of l_2 on parasitic capacitance decreases when l_2 increases to $1.4 \mu\text{m}$, and the effect of l_3 on resistance can be neglected when the number of vias reaches 7. So far, we cannot determine the optimal size of the SBD, because the simulation results are only a part of the total resistance and capacitance of the SBD. Next, we need to take the changed part into the total impedance and capacitance, and then substitute it into Eq. 1 to get the most suitable size of the SBD.

2 Chip testing and result analysis

The designed SBDs are fabricated in SMIC 180 nm process, shown in Fig. 4. The DC characteristics are measured by using Agilent B1500A semiconductor parameter analyzer, and the S-parameters are measured by using Agilent E8363B vector network analyzer. When l_s and l_1 take the minimum value of process, $l_2=1.4 \mu\text{m}$ and $l_3=\text{via5}$, the series resistance (R_s) and diode capacitance (C_0) of 8 SBD are 20Ω and 10 fF respectively measured by open-short method^[15]. The test results of eight parallel SBD are shown in Fig. 5.

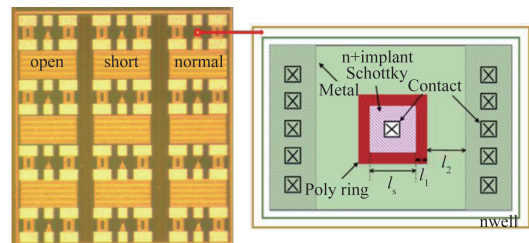


Fig. 4 Chip physical photo and the SBD plane diagram
图4 芯片照片和二极管平面示意图

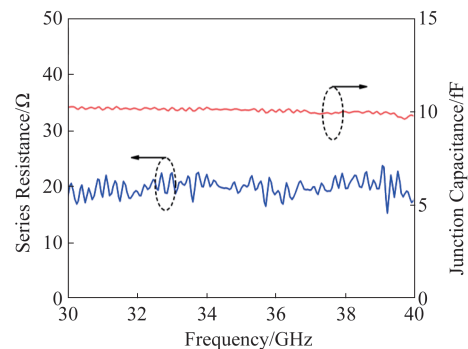


Fig. 5 Measured R_s and C_0 for the 8 cells Schottky barrier diode
图5 8个并联肖特基二极管的 R_s 和 C_0 测试结果

Based on the measured results, the simulation results are brought into the above results and normalized to

calculate the cut-off frequency F_T , which represents the ratio of the cut-off frequency to the cut-off frequency at $l_2=1.4 \mu\text{m}$ and $l_3=\text{via5}$, shown in Fig. 6.

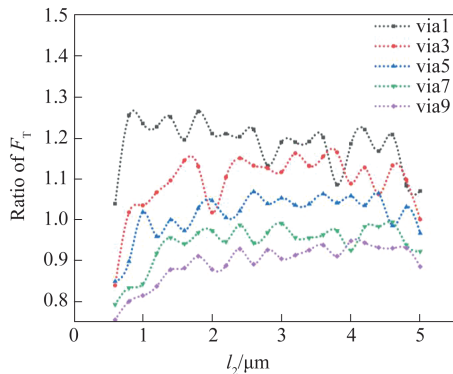


Fig. 6 Changes in ratio of F_T with l_2 and l_3
图6 不同 l_2 和 l_3 下的归一化截止频率 F_T

As we can see from Fig. 6, the diode has the highest cut-off frequency in the current process when l_3 is via1 and l_2 is between $1 \mu\text{m}$ to $2 \mu\text{m}$. According to Eq. 1, the cut-off frequency is about 800 GHz when $l_2=1.4 \mu\text{m}$ and $l_3=\text{via5}$, and the optimal design scheme can reach about 1 THz when $l_3=\text{via1}$ and $l_2=1\sim 2 \mu\text{m}$.

The comparison of previous work is shown in Table. 1. It can be seen that the work of this paper is on the leading level in same technology. But the cut-off frequency of diode will be greatly improved with the improvement of technology, which also indicates that CMOS technology has great potential in terahertz field.

Table 1 Comparison of previous works

Process	Cut-off frequency	Article
CMOS 0.18 μm	700 GHz	[13]
CMOS 0.13 μm	1.2~1.5 THz	[16]
CMOS 0.18 μm	400 GHz	[17]
CMOS 0.18 μm	800 GHz~1 THz	This

3 The detector and imaging test

The detector consists of on-chip antenna, matching circuit and SBD, shown in Fig. 7. The silicon lens used

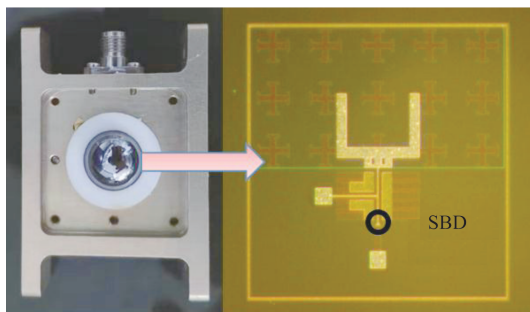


Fig. 7 Photographs of the detector package box and the Chip
图7 检波器盒体照片和芯片照片

to further increase gain is packaged with the chip forming the final imaging unit. It is calculated through testing that the antenna gain at 220 GHz is 32 dB, in which the contribution of lens is about 22 dB. The tested responsivity of the detector could achieve 130 V/W and the noise equivalent power is estimated to be $400 \text{ pW}/\sqrt{\text{Hz}}$.

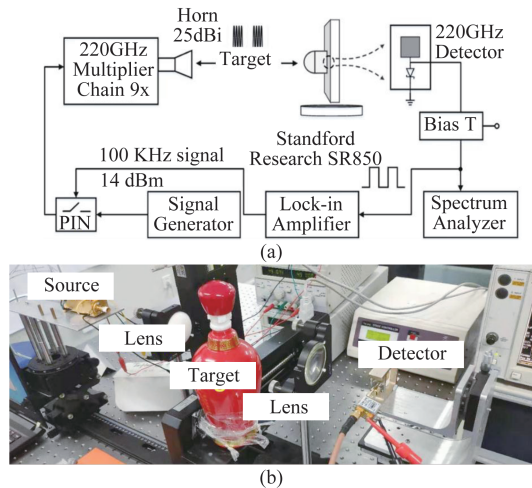


Fig. 8 Imaging test system (a) the 220 GHz imaging test setup, (b) the photo of 220 GHz imaging platform
图8 成像测试系统 (a) 220 GHz 成像系统框图, (b) 220 GHz 成像平台照片

Figure 8 shows the imaging test setup and the photo of imaging platform using the designed detector. A multiplier chain driven by signal source (Agilent E8257D) forms terahertz transmitter. When the output power of the signal source is 14 dBm, the maximum output power of the multiplier chain is 12 dBm. A detector is used to receive THz waves passing through the target. And a lock-in amplifier measures the rms value of output voltage for the detector and generates 100 KHz signals for amplitude-modulation (AM) at 220 GHz. The DC drifts and low frequency noise $1/f$ are eliminated.

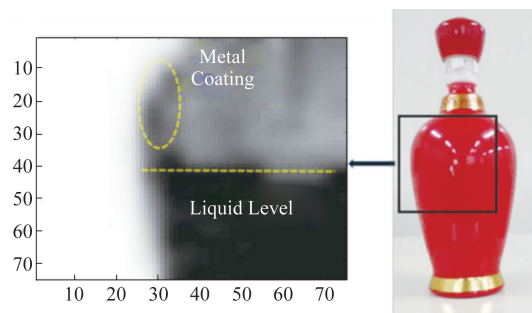


Fig. 9 Imaging results of liquid level in a ceramic bottles
图9 陶瓷瓶内液面成像结果

4 Conclusion

In the same process, polysilicon gate separation SBD has higher cut-off frequency than shallow trench isolation SBD. When designing polysilicon gate separation SBD in SMIC 180 nm process, the number of vias in

cathode should be as few as possible to increase cut-off frequency. For polysilicon gate separation SBD, when the number of vias constituting the cathode is 1 and the distance between the cathode and the polysilicon is 1~2 μm , the cut-off frequency is the highest, which is about 1 THz. The liquid level imaging experiment in ceramic bottle proves that THz wave has great potential in invisible object detection for its good penetration.

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