

## A simple approach to obtain 2.0 $\mu\text{m}$ GaSb laser by using high-order distributed Bragg reflector

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**Abstract:** GaSb-based DBR lasers with high-order Bragg gratings are fabricated without complex process. The 16<sup>th</sup>-order and 24<sup>th</sup>-order Bragg gratings are fabricated with double-trench ridge waveguide by using standard contact optical lithography respectively. The 16<sup>th</sup>-order Bragg grating laser achieves single longitudinal mode continuous-wave (CW) operation at room temperature with side mode suppression ratio (SMSR) as high as 17.5 dB. The maximum single mode continuous-wave output power is more than 10 mW at room temperature. The laser shows a very excellent wavelength stability against injection current. The single spatial mode operation is maintained in the entire injection current range. The 24<sup>th</sup>-order Bragg grating laser even shows a side mode suppression ratio up to 22.5 dB at room temperature. The emission wavelength is around 2.0  $\mu\text{m}$ .

**Key words:** laser diodes, quantum well, infrared

**PACS:** 42.55.Px, 78.55.Cr, 78.67.De

## 利用高阶 DBR 实现简单的 2.0 $\mu\text{m}$ GaSb 激光器

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**摘要:**利用高阶 Bragg 光栅成功制备出 GaSb 基 DBR 激光器, 避免了复杂的制备工艺. 利用标准接触曝光制备出 16 阶和 24 阶 Bragg 光栅以及双沟脊条波导结构. 16 阶 Bragg 光栅器件在室温下实现了 SMSR 高达 17.5 dB 的单模激光输出. CW 状态下室温最大单模输出功率超过 10 mW. 随着注入电流变化, 器件表现出出色的波长稳定性. 在整个注入电流范围内, 器件都保持单横模工作状态. 24 阶 Bragg 光栅器件室温 SMSR 为 22.5 dB. 器件的激光波长都在 2.0  $\mu\text{m}$  左右.

**关键词:**激光二极管; 量子阱; 红外

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### Introduction

Semiconductor laser diodes emitting wavelength around 2.0  $\mu\text{m}$  are attracting more and more attention recently due to a wide variety of applications ranging from remote gas sensing, free-space communication, medical and defense applications<sup>[1-5]</sup>. Currently the research of

semiconductor laser is mainly based on GaAs and InP substrates. The processing methods for these materials are well-developed. Unfortunately, the emission wavelength range around 2.0  $\mu\text{m}$  is difficult to obtain from these materials<sup>[6]</sup>. However, a variety of molecules such as CH<sub>4</sub> and CO<sub>2</sub> have strong absorption lines in this wavelength region, making the lasers emitting at 2.0  $\mu\text{m}$  wavelength region very important for atmospheric green-

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house gas sensing<sup>[7]</sup>. Thus, GaSb-based lasers which can be realized with emission wavelengths above 1.8  $\mu\text{m}$  for room temperature operation draw more and more interest. The recent research works of GaSb laser focus mainly on expanding the wavelength<sup>[8-10]</sup>, increasing the output power and efficiency<sup>[1,5]</sup> or optimizing the modal quality<sup>[11-12]</sup>. Moreover, Zhuo Deng *et al.* have investigated the effects of p-type beryllium (Be) doping on the optical properties of GaSb epilayers recently. Their research results suggest an improved optical quality in the Be-doped GaSb layer<sup>[13]</sup>. The electrical properties have been further studied as well. V. H. Compeán-Jasso *et al.* have demonstrated a very high abrupt breakdown voltage as high as 38 V of the p-GaInAsSb/n-GaSb junction<sup>[14]</sup>. These results of the GaSb laser demonstrate a significant superiority among many choice to obtain 2.0  $\mu\text{m}$  emission, benefiting from their low cost, small size and excellent laser properties.

As for accurate gas sensing, the lasers must have narrow spectral linewidth, good beam quality and moderate tuning range, meaning that the lasers must attain single longitudinal and spatial mode operation<sup>[6]</sup>. To limit the operation of the device to a fundamental spatial mode, narrow ridge waveguide defined by a small effective refractive index step  $\Delta n$  is widely employed. As for single longitudinal mode operation, the distributed Bragg reflector (DBR) is widely used. But there is a very great challenge due to the difficulty of device fabricating process, especially DBR fabricating. Several different approaches can be used for making Bragg gratings, such as e-beam lithography (EBL)<sup>[15]</sup>, interference lithography<sup>[16-17]</sup>, and nanoimprint lithography<sup>[4,6]</sup>. EBL is expensive and inefficient, leading costly and time consuming. Although interference lithography and nanoimprint lithography are good at defining Bragg gratings on surface, making the high aspect ratio etching challenging. All of them have different disadvantages among cost, efficiency, or process<sup>[17]</sup>. And some of them must divide the fabrication of Bragg grating and ridge waveguide into two steps, making the process more complex. Thus, we want to find a simple path to obtain single longitudinal operation, which makes use of high-order Bragg grating to relax the fabrication process.

In this letter, we report high-order DBR lasers whose Bragg gratings and ridge waveguide are patterned in one step, utilizing standard contact optical lithography in combination with inductively coupled plasma (ICP) etching techniques. This makes the fabricating process predigest significantly. The GaSb-based DBR lasers are manufactured with two different order Bragg gratings. Both of them show good single longitudinal and spatial mode performance around 2.0  $\mu\text{m}$ .

## 1 Device design and fabrication

The laser structure was grown on a (100) oriented n-type GaSb substrate via solid source molecular beam epitaxy (MBE). The laser structure contains a GaSb buffer layer followed by a 2.0  $\mu\text{m}$ -thick  $\text{Al}_{0.5}\text{Ga}_{0.5}\text{As}_{0.02}\text{Sb}_{0.98}$  n-type bottom cladding layer. The undoped active structure for a wavelength around 2.0  $\mu\text{m}$  consists of a

10-nm-thick single  $\text{In}_{0.2}\text{Ga}_{0.8}\text{Sb}$  quantum well embedded in two 270-nm-thick  $\text{Al}_{0.25}\text{Ga}_{0.75}\text{As}_{0.02}\text{Sb}_{0.98}$  waveguide layers. The p-type top cladding layer is composed of 2.0  $\mu\text{m}$ -thick  $\text{Al}_{0.5}\text{Ga}_{0.5}\text{As}_{0.02}\text{Sb}_{0.98}$  layer. The entire structure ended with a 250-nm-thick heavily p-doped ( $1 \times 10^{19} \text{ cm}^{-3}$ ) GaSb contact layer to attain a good ohm contact.

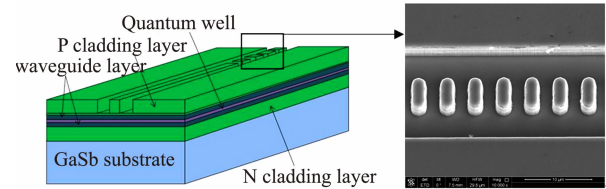


Fig. 1 Schematic layout of the DBR laser device. Inset: SEM images of DBR grating

图1 DBR激光器的示意图.插图:光栅的SEM图像

To verify the tentative performance of high-order DBR lasers, preliminary devices were processed into double-trench ridge waveguide. A 5- $\mu\text{m}$ -wide and 1500  $\mu\text{m}$ -long ridge waveguide was designed for single spatial mode operation. The 16<sup>th</sup>-order Bragg gratings have a period of 4210 nm and a grating teeth width of 2105 nm, forming a grating duty cycle of 50%. We manufactured the 16<sup>th</sup>-order Bragg grating and ridge by standard contact optical lithography simultaneously, decreasing the DBR device fabricating complexity greatly. After the MBE growth, a 400-nm-thick  $\text{SiO}_2$  was first deposited on the top of the epitaxial wafer by utilizing plasma enhanced chemical vapor deposition (PECVD) as etching protecting mask during the etching. Taking use of the hard mask and photoresist together instead of photoresist only makes the grating have steep section and stay the stable size of the pattern. The wafer was then spin-coated with photoresist. Then the grating and ridge were patterned on  $\text{SiO}_2$  layer using contact lithography and inductively coupled plasma (ICP) dry etching. The pattern transformed from  $\text{SiO}_2$  layer to epilayer using ICP dry etching,  $\text{SiO}_2$  layer working as hard mask. ICP was used for the second time to clean the residual  $\text{SiO}_2$  away. After a new 400-nm-thick  $\text{SiO}_2$  layer was deposited by PECVD on the pattern, a current injecting window on the ridge was opened using ICP dry etching. Then we sputtered Ti/Pt/Au as p-side top Ohm contact through using a magnetron sputtering system. The bottom Ohm contacts were formed by utilizing fast-annealed alloyed Au/Ge/Ni/Au after wafer thinning of GaSb substrate. After that, the devices were mounted epi-side down using indium solder on copper heat sinks.

## 2 Laser performances

The lasers were characterized after the fabricating process. The power-current-voltage ( $L-I-V$ ) characteristics of the 16<sup>th</sup>-order DBR device in the CW mode at room temperature are shown in Fig. 2. The voltage remains below 3.5 V, indicating a low series resistance. The curve of output power shows a clear threshold current of 160 mA. Even working at room temperature, an opti-

cal output power of more than 14 mW could be obtained for an injection current of 1.1 A.

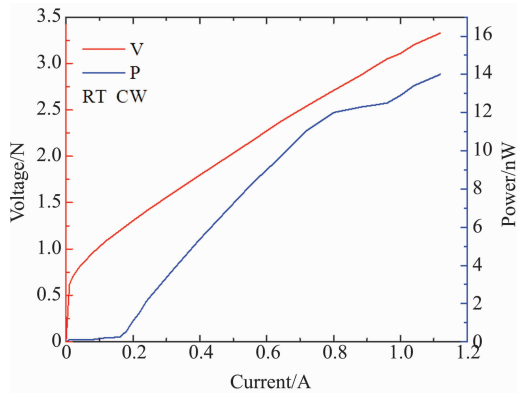


Fig. 2 Power-current-voltage characteristic of a DBR laser at room temperature

图2 室温下连续模式工作 DBR 激光器的功率—电流—电压特性曲线

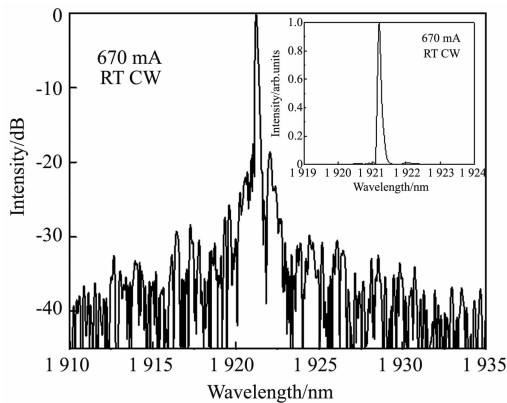


Fig. 3 Representative emission spectrum of a DBR laser with an injection current of 670 mA

图3 DBR 激光器在注入电流为 670 mA 时的激光光谱

The high-resolution emission spectrum of the 16<sup>th</sup>-order DBR laser operating with an injection current of 670 mA at room temperature is shown in Fig. 3. The emission wavelength for these conditions is 1921.2 nm. The laser shows a single longitudinal mode operation with a side mode suppression ratio (SMSR) as high as 17.5 dB, corresponding to approximately 10.3 mW optical output power. As expected, the spectrum shows stabilized emission around the predefined wavelength. The unwanted wavelengths in the gain spectrum of normal Fabry - PÉrot laser have been suppressed. Meanwhile, the wavelength which matches the DBR has a significant emission peak in the spectrum, leading single longitudinal mode operation.

The characteristics of emission spectrum and wavelength against current at room temperature are measured. Figure 4 shows the emission spectrum of the laser at each injection current. Figure 5 shows the DBR emission wavelength as a function of the injection current at room temperature. When the injection current increases from 440 mA to 1040 mA, the emission wavelength shifts from 1920.4 nm to 1922.4 nm. The slope is estimated to be

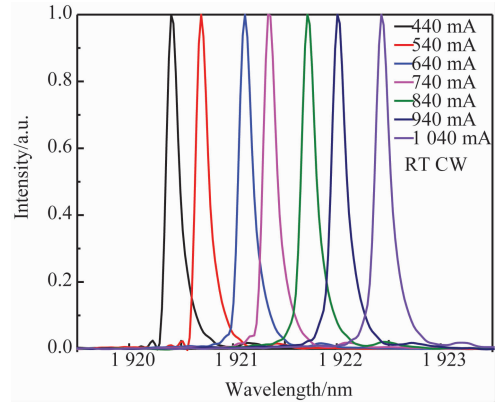


Fig. 4 Emission spectra of a DBR laser at different injection currents

图4 DBR 激光器在不同注入电流下的激光光谱

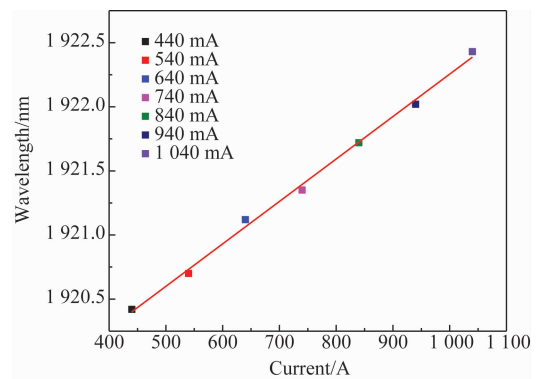


Fig. 5 Emission peak wavelengths of a DBR laser at different injection currents

图5 DBR 激光器在不同注入电流下的激光波长

about 3.3 nm/A. This slope is most likely determined by the change in effective index of the laser structure. It is much less than that of Fabry - PÉrot laser whose emission wavelength more freely follows the peak in the gain spectrum, showing a typical characteristic of DBR laser to make the wavelength stable.

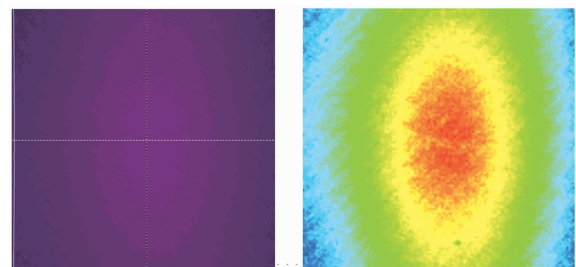


Fig. 6 Far-field images of a DBR laser. Left: measured; right: plotted by using data

图6 DBR 激光器的远场图像, 左边: 实际测量的图像; 右边: 用测量数据画的图像

Measured and plotted far-field images for the DBR laser at injection current of 0.8 A are shown in Fig. 6. The contrast and definition of the measured image are not so clear due to the low optical output power. Thus, we

plot the image by using data measured, which is defined as right of Fig. 6. It can be seen that the laser maintains single spatial mode operation.

To demonstrate the capability of DBR lasers using higher order Bragg gratings indeed, DBR lasers with 24<sup>th</sup>-order gratings were manufactured as the same process mentioned above. The 24<sup>th</sup>-order Bragg gratings have a period of 6316 nm and a grating teeth width of 3158 nm, forming a grating duty cycle of 50%. The representative emission spectrum of the 24<sup>th</sup>-order DBR laser measured at room temperature is shown in Fig. 7. The emission wavelength is 1951.3 nm. The device shows a single longitudinal mode operation with a SMSR as high as 22.5 dB at an injection current of 860 mA. There is a difference between the 16<sup>th</sup>-order DBR laser's emission wavelength and that of the 24<sup>th</sup>-order DBR laser. The difference is probably caused by the wavelength change of the maximum reflectivity for the different Bragg gratings due to the variation of the average effective index determining the Bragg wavelength. Comparing the emission spectra of the different lasers in Fig. 3 and Fig. 7, the peak's width of the 16<sup>th</sup>-order DBR laser is much less than that of the 24<sup>th</sup>-order DBR laser. The results show that the wavelength range of high reflectivity for Bragg grating may expand with their order. If the lasers work at the temperature control condition, e. g. 20°C, instead of the room temperature, the SMSR will have a significant increase.

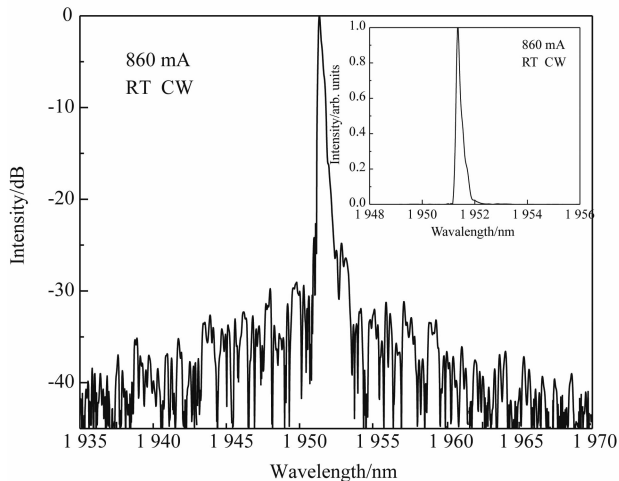


Fig. 7 Emission spectrum of the 24<sup>th</sup>-order DBR laser at 860 mA

图7 24阶DBR激光器在860 mA时的激光光谱

### 3 Conclusion

We successfully present a very simple approach to obtain 2.0  $\mu\text{m}$  single longitudinal and spatial mode operation by using high-order distributed Bragg reflector GaSb laser. The 16<sup>th</sup>-order and 24<sup>th</sup>-order gratings are patterned by using standard contact optical lithography and ICP with the ridge waveguide simultaneously, reducing the fabricating complexity sharply. The laser operates in a single longitudinal and spatial mode at room temperature with a SMSR as high as 17.5 dB. The laser's SMSR is even up to 22.5 dB. The SMSR of the laser still

has a very sufficient area to increase with the strict temperature control. The wavelength stability against current shows a typical characteristic of DBR laser. The device emits up to 10 mW at room temperature, giving the device a very significant value in mid-infrared application. The results show the capability of DBR GaSb-based lasers by using high order Bragg gratings as well.

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