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# The performance of the free-standing P(VDF-TrFE) infrared detector

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**Abstract**: Free-standing infrared detector with an Al/P(VDF-TrFE)/NiCr structure was fabricated. A semitransparent NiCr metal thin film on top of the device served as both electrode and absorption layer. The experimental results reveal that P(VDF-TrFE) has good ferroelectric and pyroelectric properties with remanent polarization 7.1  $\mu$ C/cm² and pyroelectric coefficient 27  $\mu$ C/m² K respectively. The voltage responsivity  $R_V$  and detectivity  $D^*$  of the device at 10 Hz with blackbody source temperature at 500 K are around 1 500 V/W and  $5 \times 10^7$  cmHz<sup>1/2</sup>W<sup>-1</sup>, respectively. The thermal conductance of unit area to the environment and absorption of the detector were estimated to be  $2.5 \times 10^{-3}$  W/cm² K and 0.1, respectively, from the frequency dependence of the voltage responsivity. Using the detector, the thermal image of target was obtained.

Key words: P(VDF-TrFE) film, voltage responsivity, infrared detector

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# 自支撑 P(VDF-TrFE) 红外探测器

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## Introduction

During the last several decades interests in developing uncooled infrared (IR) detectors have continuously increased [14]. Among the ferroelectric materials available, poly (vinylidene fluoride trifluoroethylene) [P(VDF-TrFE)] copolymer becomes the subject of intense research for uncooled IR detectors because of relatively high pyroelectric coefficient, low processing temperature,

easy processing on large substrate, excellent flexibility, mechanical resistance and low  $cost^{[5]}$ . It is expected that the P(VDF-TrFE) detectors will have wide applications in thermal imaging, night vision and surveillance.

In our previous studies, IR detectors with polyimide/Al/P(VDF-TrFE)/Al structure were studied<sup>[6]</sup>. In this structure, the top metal Al serves as both electrode and absorbing layer. Although good performance were obtained, optimization of the detector design was very necessary to improve their performance. For optimization

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of the detector design, several aspects must be considered<sup>[7]</sup>. Firstly, the heat capacity of the total arrangement of the detector has to be small to decrease the thermal time constant of the device. To do this, we can peel the sensor off the polyimide substrate by oxygen ion etching to form free-standing detectors. Secondly, the absorption for incoming radiation can be improved. It has been reported that NiCr film with impedance matched to that of incident infrared radiation can absorb 50% of IR radiation<sup>[8]</sup>. Thus, in this work free-standing detectors with Al/P(VDF-TrFE)/NiCr structure were fabricated. The ferroelectric, pyroelectric properties and performance of the detector were studied. Besides, the performance of free-standing detectors with Al/P(VDF-TrFE)/Al structure was also studied for comparison.

## 1 Experimental details

The detector structure is Al/P(VDF-TrFE)/NiCr. Al stripes of 120 nm thick and 0.3 mm wide were first evaporated on the polyimide substrate as the bottom electrode. P(VDF-TrFE) thin films with the composition of 70/30 mol% were prepared on Al electrodes by the spin-coating method<sup>[9]</sup>. The total P(VDF-TrFE) films are about 500 nm. Then 0.2 mm wide NiCr stripes, which serve as both top electrode and absorption layer, were fabricated onto the films to form an Al/polymer/NiCr structure. Finally, we peeled the sensors off the polyimide by oxygen ion etching to form free-standing detectors. As a comparison, free-standing Al/P(VDF-TrFE)/Al samples were also fabricated according to the processes mentioned above.

The crystal structure of the samples was analyzed by the standard x-ray diffraction (Bruker Advanced diffractometer). The polarization versus electric field (*P-E*) hysteresis loops were measured using a Radiant Precision LC system. The dielectric properties were measured using a HP4194A impedance/gain analyzer with an ac drive voltage of 0.02 V. The pyroelectric property was characterized by monitoring the dynamic pyroelectric current while the temperature of the sample is modulated periodically<sup>[10]</sup>. The voltage response of the detector to the IR radiation was measured with blackbody source temperature at 500 K and an optical chopper working at the range of 2 Hz to 80 Hz. All the measurement were carried out in ambient atmosphere.

# 2 Results and discussion

Figure 1 shows the XRD patterns for P(VDF-TrFE) film grown on Al. One diffraction peak was observed, which was assigned to the typical (110) and/or (200) of the ferroelectric  $\beta$  phase of P(VDF-TrFE)<sup>[11]</sup>. Because of the pseudohexagonal symmetry of the crystal normal to the polymer chain direction, (110) and (200) reflections overlap and cannot be resolved. Inset figure shows the polarization-electric field (*P-E*) loops for Al/P(VDF-TrFE)/NiCr samples. It is shown that well saturated *P-E* hysteresis loops are obtained, indicating P(VDF-TrFE) good ferroelectricity. The magnitude of the  $P_r$  is about 7.1  $\mu$ C/cm<sup>2</sup>.

Prior to the measurement of the pyroelectric

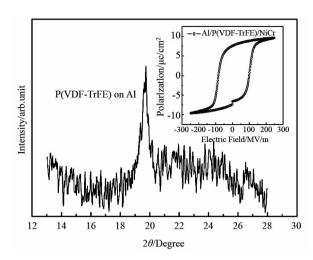


Fig. 1 XRD pattern for P(VDF-TrFE) film on Al, inset is the *P-E* loop for P(VDF-TrFE) film 图 1 生长在金属 Al 上的 P(VDF-TrFE) 薄膜的 XRD 图, 插图为 P(VDF-TrFE) 薄膜的电滞回线

coefficient, the samples were sufficiently poled. The sample temperature was modulated sinusoidally at a frequency of 0.045 Hz while the pyroelectric current was recorded by an electrometer. The measured pyroelectric coefficient of P(VDF-TrFE) is 27  $\mu$ C/m<sup>2</sup>K.

To evaluate the performance of the detectors, the voltage response of the detector was measured. Figure 2 shows the voltage responses to modulated IR radiation at 2 Hz. The frequency dependence of voltage responsivity  $R_V$ , noise and specific detectivity of the sample are shown in Fig. 3. The voltage responsivity at 10 Hz is 1 500 V/W, which is much bigger than our previous value of 209 V/W in polyimide/Al/P(VDF-TrFE)/Al detectors. As a comparison, the voltage responsivity of the later is also shown in Fig. 3.

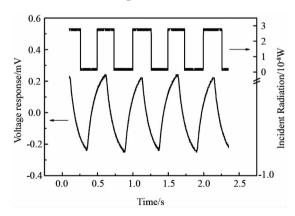


Fig. 2 Voltage response to the modulated incident radiation at 2  $\,\mathrm{Hz}$ 

图 2 调制频率为 2 Hz 时器件的电压响应

To obtain thermal time constant  $\tau_T$  and absorption coefficient  $\eta$ , the basic character parameters of the sample respectively, the frequency dependence of the voltage responsivity in Fig. 3 for the two kinds of samples is simulated using the following equations [7]

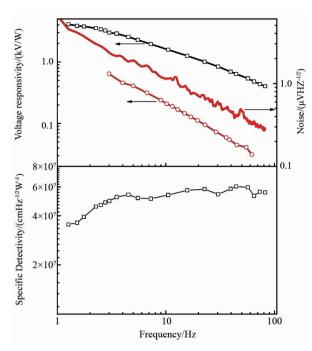


Fig. 3 The frequency dependence of voltage responsivity and noise represented by square dots and line, respectively (upper panel), and specific detectivity of detectors (lower panel). As a comparison, the voltage responsivity of Al/P(VDF-TrFE)/Al is also shown by circle dots in the upper panel.

图 3 探测器电压响应率,噪声和探测率随调制频率的变化. 上图中方块代表电压响应率,实线为噪声,下图为从电压响应率和噪声计算得到的探测率. 作为对比, Al/P(VDF-Tr-FE)/Al 器件的电压响应率也在上图中给出,数据用圆圈表示

$$R_{v} = \frac{\eta p}{k_{T}C} \frac{1}{(1 + (\omega \tau_{T})^{2})^{1/2}}, \quad (1)$$

at the middle work frequency where  $\omega \tau_E \gg 1 > \omega \tau_T$  and

$$R_{v} = \frac{\eta p}{C \sum_{i} c_{vi} d_{i}} \frac{1}{\omega} \qquad (2)$$

at high frequency where  $\omega \tau_{\scriptscriptstyle E} {\gg} \omega \tau_{\scriptscriptstyle T} {\gg} 1$  , where p is the pyroelectric coefficient of P(VD-TrFE),  $k_T$  is the thermal conductance to the environment for per unit area of the detector, C is the sum of the capacitance of detector and amplifier of the measurement circuit,  $c_{ii}$  is the specific thermal capacity for the i th layers of the device. The summation  $\Sigma$  is taken over the layers the device consists of. Based on the measured pyroelectric coefficient (27 μC/m<sup>2</sup>K), an average specific thermal capacity 2.4 J/cm<sup>3</sup> for the electrodes and P(VDF-TrFE), a thickness of 120 nm of the electrodes and the capacitance of detector (16 pF) and the amplifier (5 pF), the parameters extracted from the simulation are given in Table 1. As can be seen from the table, the first parameter  $\eta$  for Al/P(VDF-TrFE)/NiCr is 0.11, which is about three times larger than the counterpart value of 0.03 for Al/P (VDF-TrFE)/Al. This indicates better IR radiation absorbing performance of NiCr than Al films. The second parameter  $\tau_T$  for Al/P (VDF-TrFE)/NiCr is 60 ms, which is smaller than the corresponding value of 110 ms.

Besides, it is noted that the third parameter  $k_T$  are similar for both structures. Thus, it can be simply concluded that better performance of detectors can be obtained with NiCr as absorption layer. However, comparing with ideal situation, where  $k_T = 6.4 \times 10^{-3} \, \text{W/cm}^2 \, \text{K}$  and  $\eta = 1^{[12]}$ , the performance of Al/P(VDF-TrFE)/NiCr detectors in our case can be further improved by optimizing these two parameters.

Tables 1 The parameters of free-standing detector with Al/P ( VDF-TrFE )/NiCr and Al/P ( VDF-TrFE )/Al structure

表 1 Al/P(VDF-TrFE)/NiCr and Al/P(VDF-TrFE)/Al 探 测器的参数

Simulated parameters	Al/P(VDF-TrFE)/NiCr	Al/P(VDF-TrFE)/Al
η	0.11	0.03
$ au_T/\mathrm{ms}$	60	110
$k_T / (W/\text{cm}^2 K)$	$2.5 \times 10^{-3}$	2.1 × 10 <sup>-3</sup>

To further study the absorbing behavior of Al/P (VDF-TrFE)/NiCr detectors, the reflectivity of a trilayer film with the same vertical structure was measured with an FTIR spectrometer. The absorption of the device was determined from A = 1 - R - T, where A is the absorption, R the reflection, and T is the transmission of the light. In our case, the bottom electrode is thick enough, so that T = 0. The result is shown in Fig. 4. The absorption of the device is not 50% as expected for a mono metal layer with a surface resistance matched to the vacuum impedance of incident light in the measured wavelength range<sup>[8]</sup>. The interference of the lights reflected from the top and bottom electrodes at short wavelength can be observed. Thus the absorption of the sample can not be treated simply as a thin metal layer. At 6 µm, the curve reads 70%. The diffusive scattering of the light caused by the roughness of the sample surface was omitted in the above consideration, resulting in an over estimated absorption value than the actual one, especially in the short wavelength, as compared with the value of  $\eta =$ 0.1 obtained from the fitting to experimental results.

With the above single element device, thermal image has been obtained via a two dimension scanning opti-

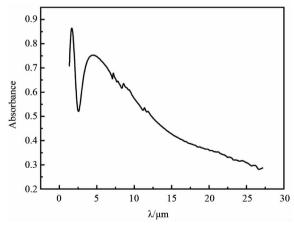


Fig. 4 Absorbance curve of Al/P(VDF-TrFE)/NiCr trilayers

图 4 Al/P(VDF-TrFE)/NiCr 三层结构的吸收曲线

cal system. Figure 5 shows the thermal image of a target. The pigtail of the girl is distinct as can be seen from the figure. Despite of these unfavorable parameters  $k_T = 2.5 \times 10^{-3}$  W/cm<sup>2</sup>K and  $\eta = 0.11$ , thermal image could be obtained benefiting from the high voltage responsibility. The performance of the detector can be further improved by increasing the absorption of the detector and decreasing the thickness of the P(VDF-TrFE), thus the thermal time constant of the device.

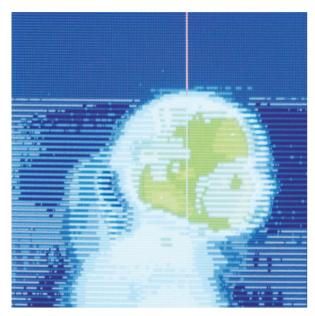


Fig5 IR image of a target with P(VDF-TrFE) detector 图 5 采用 P(VDF-TrFE) 探测器实现的目标成像图

#### 3 Conclusion

The fabricated P(VDF-TrFE) films have good ferroelectric and pyroelectric properties. Comparing with Al/P(VDF-TrFE)/Al detector, Al/P(VDF-TrFE)/NiCr sample exhibits better performance because of better NiCr absorbing behavior. The thermal conductance of unit area to the environment and absorption of Al/P(VDF-Tr-FE)/NiCr detector were  $k_T = 2.5 \times 10^{-3}$  W/cm²K and  $\eta = 0.11$ . Despite of these unfavorable parameters, good

thermal image could still be obtained. In future work, study should be done to optimize these two parameters for further improving the performance of the detector.

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